Numerical simulations of nonlinear thermally-stratified incremental spin-up in a circular cylinder

Sergey A. Smirnov\textsuperscript{a}, J. R. Pacheco\textsuperscript{b,c,1} and Roberto Verzicco\textsuperscript{d}
\textsuperscript{a}Department of Mechanical Engineering, Texas Tech University, Lubbock, TX 79409, USA
\textsuperscript{b}School of Mathematical and Statistical Sciences, Arizona State University, Tempe, AZ 85287, USA
\textsuperscript{c}Environmental Fluid Dynamics Laboratories, Department of Civil Engineering and Geological Sciences, The University of Notre Dame, South Bend, IN 46556
\textsuperscript{d}Dipartimento di Ingegneria Meccanica, Universita’ di Roma “Tor Vergata”, Via del Politecnico 1, 00133, Roma, Italy

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1 Abstract

We present a numerical study of incremental spin-up of a thermally-stratified fluid enclosed within a right circular cylinder with rigid bottom and side walls and stress-free upper surface. This investigation reveals a feasibility for transition from an axisymmetric initial circulation to non-axisymmetric flow patterns at late spin-up times. We show that the destabilizing mechanism is not purely baroclinic, but that vertical and horizontal shears may contribute to the instability. By characterizing the azimuthal instabilities without introducing any simplification we were able to assess to what extent an insulating boundary condition changes the time-dependent emergence of the instability. Our results agree with previous experimental data and provide a framework for understanding the role played by the baroclinic vorticity

\textsuperscript{1}Tel.: +1 (480) 965-8656, Fax: +1 (480) 965-1804, e-mail: rpacheco@asu.edu
in the development of instabilities in thermally-stratified incremental spin-up flows.
2 Introduction

Stratified spin-up flow – an impulsive change of the rotation rate of a rigid container filled with a liquid – is a classical fluid mechanics problem that has been extensively studied in the past (for a comprehensive review of homogeneous and stratified spin-up see[1]). Because spin-up/down flows are transient problems, they cannot be analyzed for stability in the usual sense, the final state will depend on the final density profile: the curvature of the isotherms near the bottom/top of the insulated walls results in radial diffusive mass transport and the associated Sweet-Eddington azimuthal flow [2, 3]. This is a nonlinear question where the interest is in the state of the transient flow.

One of the earliest studies of spin-up leading to the formation of cyclonic and anticyclonic eddies is due to Greenspan [4], who considered stratified fluid in a cylindrical container. The qualitative observations made in [4], were extended and quantified in the experimental investigation of [5]. Particular attention was paid to determining the criteria for axisymmetric breaking instabilities by adapting the stability analysis of [6]. The initial phase of motion in spin-up reported by [7, 5] was characterized by the formation of axisymmetric corner regions that accumulated fluid drawn through the Ekman layer. The formation of corner regions due to downwelling coupled with the non-penetration boundary conditions for density, forced the isopycnals within the central core to be displaced vertically. This vertical stretching reduced
the density gradient within the core, and its buoyancy frequency following
the establishment of the corner regions decreased. The stability of the cen-
tral vortex was observed to depend on its stratification and radius-to-height
aspect ratio. For highly stratified flows the axisymmetry was retained and
the central vortex reached a state of near solid body rotation. For relatively
low stratification, the axisymmetry of the flow was broken due to baroclinic
unstable waves that propagated along the interface of the core and corner
regions.

Similar non-axisymmetric instabilities in which cyclones near the outer
wall propagated toward the center of the tank were also observed in two-
layer stratification flows with a thin lower layer [8]. A region where the
upper layer was in direct contact with the bottom of the tank (bare spot)
was formed during the spin-up. The circular shape of the bare spot was
distorted by the presence of waves which grew to large amplitude on the
front surrounding the bare spot. The flow patterns observed by these waves
were similar to those produced by a front at the free surface of baroclinic
instabilities of Ekman layers observed by [6].

Columnar baroclinic vortices generated by the instability of stratified flu-
ids due to a change in rotation rate of its container (cylinder or annulus)
from \( \Omega_i = \Omega - \Delta \Omega \) to \( \Omega \) were reported in [9, 10, 11]. It was found that
inside the corner regions, which develop at the intersection of the vertical
sidewall and horizontal bottom boundary, the density gradients were weak
(the fluid was well-stirred), while above the corner regions the density gra-
dient was higher compared to the initial background value. The eddies grew
in size and marched along the circumference until they occupied a large por-
tion of the tank. These laboratory experiments (conducted at much later
spin-up times) have stressed the importance of both baroclinic (vertical) and
barotropic (horizontal) shears in the symmetry breaking process. But despite
the efforts to elucidate which mechanisms dominate the breakup of symme-
try, at what time, and how these mechanisms interact amongst each other
[12] they remain elusive.

On the other hand, numerical simulations of spin-up/down have limited
their investigation to the axisymmetric stage of the flow evolution [13, 14,
15, 16, 17, 18, 19, 20, 21, 22, 7, 23, 24]. Recent three-dimensional numeri-
cal simulations analyzed homogeneous swirling flows created by a differential
rotation in cylinder-lid enclosures [25, 26, 27]. However, despite the numer-
ous numerical studies on spin-up flows, three-dimensional simulations are
conspicuously lacking.

This work is concerned with the numerical investigation of nonlinear in-
cremental spin-up of a thermally-stratified fluid with kinematic viscosity $\nu$
and thermal diffusivity $\kappa$ in a cylinder of radius $R$ and height $2H$ rotating
about a vertical axis. Initially, its temperature varies linearly with height
and is characterized by a constant buoyancy frequency $N$ which is propor-
tional to the temperature gradient. The system undergoes an abrupt change
in the rotation rate from its initial value $\Omega_i = \Omega - \Delta \Omega$, when the fluid is in
a solid-body rotation state, to the final value $\Omega$. Our investigation focuses
on the regime that corresponds to the transient Ekman bottom boundary layer. Because the exact conditions for the transition to turbulence for stratified spin-up are unknown, we use the criterion of Lilly [28] to determine the region of the stability, i.e. $Re_\delta < 55$, where $Re_\delta$ is the Reynolds number based on the bottom Ekman layer depth. Laboratory experiments of [29] showed that the Ekman layer remains stable until $Re_\delta \approx 57$ and becomes fully turbulent at $Re_\delta \geq 150$. Recent measurements of the bottom friction law during homogeneous spin-up over a flat surface also confirmed these estimates [30]. We restrict our simulations to large aspect ratios and compare the instabilities arising due to different boundary conditions on the horizontal walls. We consider five different runs listed in table 1 where the following notation indicates the set of parameters used in the simulations: NEU and DIR correspond to the non-linear stratified flow with Neumann and Dirichlet boundary conditions on the horizontal walls of the cylinder respectively; HOM stands for the spin-up of a homogeneous fluid (no stratification); and LBU and SRO designate the large-Burger number and small-Rossby number runs with Neumann boundary conditions, respectively. Using Fourier analysis of the velocity field in the azimuthal direction, we were able to identify the most unstable wave number $n$ as the mode with largest growth rate. We computed the time evolution of each term of the perturbation energy equation, which allowed us to determine the contribution to the instability of the barotropic, baroclinic, centrifugal and dissipative terms. Our two objectives are to study the characteristics of the azimuthal instabilities without
Figure 1: Schematic of the fluid system. At $\hat{t} = 0$ the cylinder is instantly accelerated from the initial rotation rate $\Omega_i = \Omega(1 - \epsilon)$ to a new rotation rate $\Omega$. The inset shows the formation of the corner region during the first stage of spin-up at $\tau \approx 6$.

introducing any simplification and to determine the extent that an insulating, rather than fixed temperature, boundary condition would change the
time-dependent emergence of the instability.

The three-dimensional numerical solutions allowed us to identify the mechanism responsible for the nature of the vortex structure at the late stages of flow development when using Neumann or Dirichlet boundary conditions. The simulations show a noticeable but expected difference in stratification between isotated and constant-temperature boundary conditions (NEU and DIR), and this is accompanied by a peculiar change of the isobars, which in turn triggers different instabilities. Evidence of this conjecture is given at the end of the results section.
Table 1: Parameters used in the simulations. The dash in the table implies that the number from the previous column did not change.
3 Navier-Stokes equations and the numerical scheme

3.1 Governing equations

The system of interest consists of a circular cylinder of radius $R$ rotating counter-clockwise about its axis of symmetry with the rotation rate $\Omega_i e_z$, where $e_z$ is the unit vector pointing in the positive direction of the $\hat{z}$ axis (see figure 1). We consider the case when the gravity and rotation vectors are colinear, i.e., $g = -ge_z$. The fluid occupies the domain $0 \leq \hat{r} \leq R$, $0 \leq \hat{z} \leq 2H$, so that the total height of the cylinder is $2H$. At time $\hat{t} = 0$ the system is instantly accelerated by the amount $\Delta\Omega$ to a new rotation rate $\Omega$ from its initial state $\Omega_i = \Omega(1 - \epsilon)$, where $\epsilon = \Delta\Omega/\Omega$. We describe the fluid motion relative to the cylindrical coordinate system $\hat{r} = (\hat{r}, \hat{\theta}, \hat{z})$ rotating with the final rotation rate $\Omega$. The components of the velocity vector $\hat{u} = (\hat{u}_r, \hat{u}_\theta, \hat{u}_z)$ represent the radial, azimuthal and vertical velocities respectively with respect to this frame. Note that in this reference frame, the final state will depend on the final density profile: the curvature of the isotherms near the bottom/top of the insulated walls results in radial diffusive mass transport and the associated Sweet-Eddington azimuthal flow [2, 3].

The governing equations which describe the motion of an incompressible flow of density $\rho$ in the rotational (non-inertial) reference frame in the Boussi-
nesq limit have the following form [31, 32]

\[ \nabla \cdot \hat{u} = 0, \]  
(1a)

\[ \frac{D\hat{u}}{Dt} + 2\Omega \times \hat{u} = -\frac{1}{\rho_o} \hat{\nabla} \hat{p} - \frac{\rho}{\rho_o} g e_z + \frac{\rho}{\rho_o} \Omega^2 \hat{r} e_r + \nu \hat{\nabla}^2 \hat{u}, \]  
(1b)

\[ \frac{D\hat{T}}{Dt} = \kappa \hat{\nabla}^2 \hat{T}. \]  
(1c)

A temperature difference of 20°C allow us to retain the Boussinesq approximation in the governing equations [33], where any variations in the physical properties of fluid (water) with temperature were considered negligible. In all cases the sidewall of the cylinder is thermally insulated.

In the equations above \( \hat{p} \) and \( \hat{T} \) are the total pressure and temperature functions respectively, while \( \rho_o \) is the mean density of the fluid. The unit vector \( e_r \) points in the positive \( \hat{r} \)-direction. The kinematic viscosity and thermal diffusion coefficients are \( \nu \) and \( \kappa \) respectively and the material derivative operator is defined as \( \frac{D}{Dt} = \partial/\partial \hat{t} + \hat{u} \cdot \hat{\nabla} \), where \( \hat{\nabla} \) is the vector differential operator. We assume that the non-inertial reference frame does not accelerate as a whole and its angular acceleration is zero (constant rotation rate). We do not make any a-priori assumptions about the magnitude of the centrifugal acceleration term in (1b).

We consider the case of a stable linear background density stratification characterized by the buoyancy frequency squared

\[ N^2 = -\frac{g}{\rho_o} \frac{d \rho_b}{d \hat{z}} = \text{constant} > 0, \]  
(2)
so that the background density profile is

\[ \rho_0(\hat{z}) = \rho_o \left( 1 - \frac{N^2}{g} \hat{z} \right). \]  \hspace{1cm} (3)

In the case of a thermal stratification, the relationship between the fluid temperature and density is given by the equation of state

\[ \rho = \rho_o \{ 1 - \alpha (\hat{T} - \hat{T}_o) \}, \]  \hspace{1cm} (4)

where \( \alpha \) is the coefficient of thermal expansion, and \( \hat{T}_o = \text{constant} \) is the reference temperature. Initially the top and bottom horizontal surfaces of the cylinder are kept at constant temperature, so that the total temperature difference \( 2\Delta \hat{T} \) occurs over the height \( 2H \). The square of the buoyancy frequency (2) becomes

\[ N^2 = \alpha g \frac{\Delta \hat{T}}{H} > 0, \]  \hspace{1cm} (5)

while the background temperature profile is

\[ \hat{T}_b(\hat{z}) = \hat{T}_o + \frac{\Delta \hat{T}}{H} \hat{z} = \hat{T}_o + \frac{N^2}{\alpha g} \hat{z}, \]  \hspace{1cm} (6)

so that \( \hat{T}_o + 2\Delta \hat{T} \) and \( \hat{T}_o \) are the temperature values at the top and bottom boundaries respectively. In this study, we focus on the case of an open fluid domain (free upper surface), assuming the stress-free condition at the top (effects of surface tension and deformation are neglected). The total pressure and temperature functions are defined as \( \hat{p} = \hat{P} - \rho_o g \hat{z} + \rho_o (\Omega \hat{r})^2 / 2 \) and \( \hat{T} = \hat{T}_o + \hat{T}_H \), where \( \hat{P} \) and \( \hat{T}_H \) are the reduced pressure and temperature functions respectively. If we scale the space variables \( \hat{r}, \hat{z} \) with the characteristic length
$H$, the velocity components with the characteristic velocity $\Delta \Omega H = \epsilon \Omega H$, the pressure $\hat{P}$ with $2\Omega^2 \Delta H^2 \epsilon \rho_0$, the temperature $\hat{T}_H$ with $2\Delta \hat{T}$, and the time $\hat{t}$ with $(2\Omega)^{-1}$, the governing equations in dimensionless form can be written as

\begin{align}
\nabla \cdot \mathbf{u} &= 0, \\
\frac{\partial \mathbf{u}}{\partial \hat{t}} + \frac{\epsilon}{2} \mathbf{u} \cdot \nabla \mathbf{u} &= -\nabla \hat{P} + \frac{4B^2}{\epsilon} \hat{T}_H \mathbf{e}_z - \mathbf{e}_z \times \mathbf{u} - \frac{8FB^2}{\epsilon} \hat{T}_H \mathbf{e}_r + E \nabla^2 \mathbf{u}, \\
\frac{\partial \hat{T}_H}{\partial \hat{t}} + \frac{\epsilon}{2} \mathbf{u} \cdot \nabla \hat{T}_H &= \frac{E}{\sigma} \nabla^2 \hat{T}_H.
\end{align}

The initial and boundary conditions become

\begin{align}
\mathbf{u}_r &= u_z = 0, \quad u_\theta = -r, \quad \hat{T}_H = \frac{z}{2}; \quad \text{at} \quad \tau = 0, \\
\mathbf{u}_r &= u_\theta = u_z = 0; \quad \text{at} \quad z = 0, \\
\frac{\partial \mathbf{u}_r}{\partial \hat{z}} &= \frac{\partial u_\theta}{\partial \hat{z}} = \frac{\partial u_z}{\partial \hat{z}} = 0; \quad \text{at} \quad z = 2, \\
\mathbf{u}_r &= u_\theta = u_z = 0, \quad \frac{\partial \hat{T}_H}{\partial \hat{r}} = 0; \quad \text{at} \quad \hat{r} = \Gamma.
\end{align}

The top and bottom walls are either maintained at constant temperatures (Dirichlet boundary conditions)

\begin{align}
\hat{T}_H &= 0, \quad \text{at} \quad z = 0, \\
\hat{T}_H &= 1, \quad \text{at} \quad z = 2,
\end{align}

or are insulated (Neumann boundary conditions)

\begin{align}
\frac{\partial \hat{T}_H}{\partial \hat{z}} &= 0 \quad \text{at} \quad z = 0, 2.
\end{align}
In the equations above, $\epsilon = \Delta \Omega / \Omega$ is the Rossby number, $E = \nu / 2\Omega H^2$ is the Ekman number, $B = N / 2\Omega$ is the stratification parameter, $\sigma = \nu / \kappa$ is the Prandtl number, $\Gamma = R / H$ is the aspect ratio, and $F = \Omega^2 H / 2g$ is the rotational Froude number. The non-dimensional rotation period is defined as $\tau = \Omega \hat{t} / 2\pi = t / 4\pi$ which will be used to present the results.

We characterized the azimuthal perturbations using the energy equation. In the system of governing equations (7) we decompose all variables into axisymmetric and non-axisymmetric parts. The axisymmetric part represents the mean flow (averaged quantities on the azimuth), while the non-axisymmetric part corresponds to the flow perturbations [34]. Thus, any quantity in (7) can be expressed as

$$q(r, \theta, z) = \bar{q}(r, z) + q'(r, \theta, z), \quad (11)$$

where

$$\bar{q}(r, z) = \frac{1}{2\pi} \int_0^{2\pi} q(r, \theta, z) \, d\theta. \quad (12)$$

Substituting (11) into the momentum equation (7b), taking the dot product with $u'$ and integrating over the entire domain $V$, yields the energy equation for the azimuthal disturbances

$$\frac{d\epsilon}{dt} = \frac{d}{dt} \int_V \frac{1}{2} |u'|^2 \, dV = -\frac{\epsilon}{2} \int_V \mathbf{u}' \cdot (\mathbf{u}' \cdot \nabla \mathbf{u}) \, dV + \frac{4B^2}{\epsilon} \int_V T_H u'_z \, dV$$
$$-\frac{8FB^2}{\epsilon} \int_V T_H r u'_r \, dV - E \int_V |\nabla u'|^2 \, dV.$$  \quad (13)

$$= \sum_{i=1}^{4} H_i$$

13
The left-hand-side of (13) represents the kinetic energy growth rate of the azimuthal disturbance due to $(H_1)$ shear of the mean axisymmetric flow (barotropic production); $(H_2)$ conversion of gravitational potential energy (baroclinic production); $(H_3)$ conversion of centrifugal potential energy; and $(H_4)$ viscous dissipation (it is always a sink for the kinetic energy of disturbances).

One global measure we have used to characterize the various solutions obtained is the kinetic energy in the $n$th Fourier mode of the solution:

$$E_n = \frac{1}{2} \int_{r=0}^{\Gamma} \int_{z=0}^{z=2} \mathbf{u}_n \cdot \mathbf{u}_n^* r \, dr \, dz,$$

where $\mathbf{u}_n$ is the $n$th Fourier mode of the velocity field and $\mathbf{u}_n^*$ is its complex conjugate.

### 3.2 Numerical method

The governing equations (7)–(10) are discretized on a staggered grid with the velocities at the faces and all the scalars in the center of the computational cell; the resulting system of equations is solved by a fractional-step method. The discretization of both viscous and advective terms is performed by second-order-accurate central finite-difference approximations. The elliptic equation, necessary to enforce incompressibility, is solved directly using trigonometric expansions in the azimuthal direction and the tensor-product method [35] for the other two directions. Temporal evolution is via a third-order Runge–Kutta scheme which calculates the nonlinear terms explicitly.
and the viscous terms implicitly. The stability limit due to the explicit treatment of the convective terms is \( \text{CFL} < \sqrt{3} \), where CFL is the Courant, Friedrichs and Lewy number. A useful feature of this scheme is the possibility to advance in time by a variable time step, without reducing the accuracy or introducing interpolations. The three-dimensional simulations listed in table 1 were conducted using uniform grids in the azimuthal direction and non-uniform grids in the radial direction and axial direction with clustering at the walls. We have varied \( \delta t \) in all the simulations in this paper such that the local CFL \( \leq 1.5 \), where \( \text{CFL} = \left( \frac{|u_r|/\delta r + |u_\theta|/(r\delta \theta) + |u_z|/\delta z}{\delta t} \right) \), with the velocity components averaged at the center of each computational cell, then the smallest such determined local \( \delta t \) is used for time advancement. At least 10 grid points were placed inside the bottom Ekman and sidewall boundary layers respectively. For most of the runs, \( n_\theta \times n_r \times n_z = 96 \times 351 \times 151 \) grid points were used in the azimuthal radial and axial directions respectively. One run was made with \( n_\theta \times n_r \times n_z = 192 \times 601 \times 251 \) in order to verify the grid-independence results during the axisymmetric stage of the flow and to test the adequacy of the coarser grid in resolving all the relevant flow scales.

Various test problems were also used for the verification of the numerical code. In particular, for the spin-up in a cylindrical container of height \( 2H \), figure 2 shows a comparison between experimental results for the azimuthal velocity \( \hat{u}_\theta \) at mid-depth \( H \) and the corresponding numerical results of our code. The numerical results were in excellent agreement with the experimen-
Figure 2: Comparison of stratified spin-up experiments with numerical simulations for the azimuthal velocity \( \hat{u}_\theta \) with Dirichlet and Neumann boundary conditions. (a) Parameters: \( 2H = 6 \text{ cm}, \ R = 9.5 \text{ cm}, \ N = 0.97 \text{s}^{-1}, \ \Omega = 0.384 \text{s}^{-1}, \ ST^{-1}(= NH/2\Omega_i R) = 0.49, \ E(= \nu/2\Omega_i H^2) = 7.24 \times 10^{-4}, \ \epsilon(= \Delta \Omega/\Omega_i) = 0.222 \) and \( \Omega_i = 0.314 \text{s}^{-1}. \) The vertical and radial locations are at the mid-depth \( \hat{z} = H \) and \( \hat{r}/R = 0.64. \) The dashed lines (– –) correspond to the numerical simulations of [19]; the circles (○) to the laser-Doppler measurements of [19]; and the solid lines (—–) to our numerical simulations. (b) The fluid depth is \( 2H = 20 \text{ cm}, \) tank radius \( R = 46 \text{ cm} \) and the buoyancy frequency is \( N = 1.35 \text{ s}^{-1}. \) The spin-up sequence is \( \Omega = 0.2 \rightarrow 0.4 \text{ s}^{-1} (\epsilon = 0.5) \) at \( \hat{t} = 270 \text{ s}^{-1}. \) The vertical position is \( \hat{z} = H. \) The symbols (+) are the results of laboratory measurements of [9], and the dashed lines (– –) are our numerical simulations.
tal results of [19] for thermal stratification (Dirichlet boundary conditions) and [9] for salinity stratification (Neumann boundary conditions). We have also performed similar checks as in [34] who studied a different but related problem of baroclinic instabilities in the presence of rotation and stratification.

4 Results

4.1 Axisymmetric spin-up

In this section we consider three different sets of parameters where the flow remained axisymmetric throughout the spin-up process. We consider highly stratified flow LBU, strong rotational effects (small Rossby number) with thermal stratification SRO, and homogeneous flow HOM with parametric values listed in table 1. In all cases the sidewall and top/bottom walls of the cylinder are thermally insulated.

Figure 3 depicts the evolution of the temperature field for LBU and SRO (see movies 1 and 2 available online). The formation of the corner regions at early states of flow development is shown at $\tau \approx 1$. After the corner regions form, the fluid flushes back towards the center of the tank and the stratification near the axis $r = 0$ decreases. For LBU the state at $\tau = 85$ shows a three-layer structure, i.e. a stratified layer bounded above and below by mixed fluid. The final state of solid body rotation is delayed in SRO when compared to LBU.

Figure 4 shows the evolution of vertical vorticity for LBU at three levels
(a) Case LBU. The region shown is $r \in [0, 2.33]$ and $z \in [0, 2]$ (not to scale).

(b) Case SRO. The region shown is $r \in [0, 6.67]$ and $z \in [0, 2]$ (not to scale).

Figure 3: Isotherms on the planes $\theta = 0 - \pi$. At $\tau = 0$ there are 32 linearly spaced contour levels in the range $T_H \in [0, 1]$. Movies 1 and 2, available in the online version, show the spatio-temporal characteristics for the isotherms on the planes $\theta = 0 - \pi$ over several rotation periods at a rate of 10 frames per second, with each frame being 1 rotation period apart.
Figure 4: Case LBU: Axial vorticity $\omega_z$; there are 7 positive (solid/black) and 7 negative (white/dashed) linearly spaced contour levels in the range $\omega_z \in [-1, 1]$. The region shown is $r \in [0, 2.33]$ and $z \in [0, 2]$.

Figure 5: Case SRO: Axial vorticity $\omega_z$. There are 7 positive (solid/black) and 7 negative (white/dashed) linearly spaced contour levels in the range $\omega_z \in [-1, 1]$. The region shown is $r \in [0, 2.33]$ and $z \in [0, 2]$. Movies 3-5, available in the online version, show the spatio-temporal characteristics for the vertical vorticity.
$z = 0.01, 0.25$ and $1.0$. In this case the aspect ratio of the cylinder is almost three times smaller in this case ($\Gamma = 2.33$) compared to LBU and HOM ($\Gamma = 6.67$). The vorticity distribution at early times ($\tau < 10$) consists of a system of annular bands of vorticity which changes sign from one location to another. The system never breaks the axial symmetry, slowly advancing towards the state of a new solid-body rotation. The vorticity pattern at $\tau = 85$ for LBU is not shown because of the miniscule values of $\omega_z$ at that time.

The evolution of axial vorticity $\omega_z$ for SRO shown in figure 5 and movies 3-5, is similar to the LBU case, but with one important distinction: at around $\tau = 20$, the flow tends to break the symmetry at the lower $z$-levels ($z < 1$). A wavy perturbation with multiple inflection points propagates along the temperature front at some distance from the outer sidewall (see movies 3-5). Its amplitude grows in time, but there is no cascade towards large-scale vortices that would permanently break the symmetry of the flow. After $\tau \sim 40-45$, the spin-up flow ‘re-laminarizes’ and the vorticity isolines acquire a circular shape (figure 5, $\tau = 60$).

The spin-up simulations for a homogeneous fluid (HOM) for the set of parameters listed in table 1 did not develop small-scale instabilities near the outer wall nor large-scale eddy formation at late times on any horizontal plane despite that a large amount of horizontal shear $\Delta \Omega$ was initially transferred to the fluid. Clearly, for other values of the parameter set we could expect that eddies or turbulence could occur for a homogeneous fluid.
4.2 Nonaxisymmetric spin-up with insulating boundary conditions: Case NEU

The evolution of the temperature field on the planes $\theta = 0 - \pi$ over several rotation periods is shown in figure 6 for $(\Gamma, \epsilon, Bu) = (6.67, 0.727, 0.379)$ with the top and bottom walls insulated. During spin-up, the isotherms around the corner regions deform due to the Ekman transport in the bottom boundary layer towards the outer sidewall. A similar transport in the upper part of the fluid domain is absent because of the imposed free-surface (stress-free) boundary condition. Pockets of cold and warm fluid form isotherms with rounded configurations inside the fully-developed corner regions depicted in figure 6 at $\tau = 7$. The downwelling motion in the central part of the cylinder coupled with the insulating boundary conditions for temperature, force the isotherms around $r = 0$ to be displaced vertically ($\tau \approx 7$). The maximum height and radius of the corner regions are approximately $h_{NEU} \approx 1.68$ and $L_{NEU} \approx 4$ and these are consistent with the theoretical estimates $h = 2/3Bu (= 1.74)$ and $L = 2\Gamma/3 (= 4.44)$ of [7]; the time to formation is $\tau \approx 7.7$ rotation periods.

For homogeneous fluids the spin-up time is $\tau_{su} = (2E)^{-1/2}/\pi \approx 6$ whereas [7] found that the corner regions mature until a time $\tau_{su} = 1.3/(\Gamma \sqrt{2EN}) \approx 9.8$ rotation periods.

The collapse of the corner regions is accompanied by the generation of internal waves revealed in the undulation of the isotherms ($\tau = 34$). At late times, the temperature gradient has decreased and the state at $\tau = 85$ shows the development of a stratified layer bounded above and below by relatively
Figure 6: Case NEU: Isotherms on the planes $\theta = 0 - \pi$; at $\tau = 0$ there are 15 linearly spaced contour levels in the range $T_H \in [0, 1]$ showing the formation of the corner regions and the motion after the vortex core is formed. The region shown is $r \in [0, 6.67]$ and $z \in [0, 2]$. Movie 6, available in the online version, shows the spatio-temporal characteristics for the isotherms on the planes $\theta = 0, \pi$ over 145 rotation periods at a rate of 10 frames per second, with each frame being 1 rotation period apart.
Figure 7: Case NEU: Radial velocity $u_r$ and temperature profiles $T_H$ at different radial locations and $\theta = 0$. Note that the solid line in (a) indicates the depth of the Ekman layer.
Figure 8: Case NEU: Temperature and vortex structure identified by the iso-surfaces of $Q = 0$ colored by temperature. The figures on the left correspond to $T_H \in [0 - 1]$ and on the middle/right to the vortex structure. The region shown is $r \in [0, 6.67]$ and $z \in [0, 2]$. Movie 7, available in the online version, shows the spatio-temporal characteristics for the isotherms and vortex structure. The animations run over 100 rotation periods at a rate of 4 frames per second, with each frame being 1 rotation period apart.
Figure 9: Case NEU: Axial vorticity $\omega_z$; there are 7 positive (solid/black) and 7 negative (white/dashed) linearly spaced contour levels in the range $\omega_z \in [-1, 1]$. Movies 8-10, available in the online version, show the spatio-temporal characteristics for the axial vorticity at different $z$-levels.

Figure 10: Case NEU: Time evolution of different energy modes $E_n$: $n = 0$ (---); $n = 1$ (○); $n = 2$ (– –); $n = 3$ (– · –); $n = 4$ (⋄).
Figure 11: Case NEU: (a) Time evolution of (a) $H_i$-terms in the rate of change of kinetic energy of azimuthal perturbations, barotropic term $H_1$ (— —); baroclinic term $H_2$ (– · –); centrifugal term $H_3$ (– –); viscous dissipation term $H_4$ (– · · –), (b) the rate of change of kinetic energy $de/dt$ and (c) the kinetic energy $e(\tau)$. 
well-mixed fluid (see movie 6 in the online version of the paper).

The formation and development of the Ekman bottom boundary-layer flow at \((r, \theta) = (5.5, 0)\) is depicted in figure 7(a) where the horizontal solid line marks the thickness of the Ekman layer \(\delta\). The vertical profiles of the radial velocity \(u_r\) show an increased fluid transport in the meridional plane at early spin-up times \((\tau \leq 1)\) followed by a gradual decrease in both, the Ekman transport and amplitude of \(u_r\). The value of \(u_r\) decreases near \(z = 0\) at about 18-20 rotation periods as the entrainment of the interior fluid into the bottom Ekman layer shuts down. Figures 7(b)-(d) illustrate the vertical profiles of temperature \(T_H(z)\) on the plane \(\theta = 0\) for \(r = 0.1, 4.5\) and 6.5.

The dashed lines in the figures depict the background temperature profile at time \(\tau = 0\). Near the axis of rotation \((r = 0.1)\) the temperature profiles for \(\tau > 0\) lie beneath the initial temperature contour, implying that during spin-up the inner part of the cylinder experiences a strong downwelling event. The largest deviation from the initial linear profile occurs after about 18-20 rotation periods. The temperature continuously varies along the top and bottom boundaries of the cylinder due to the thermally-insulated boundaries.

The Ekman boundary layer homogenizes in the corner regions as well as near the center. At very late times \((\tau \sim 120)\) the shape of the isotherms deviates significantly from its initial linear profile, indicating that significant mixing has occurred in the system, i.e., the vertical profile for \(T_H\) plotted at different radial locations are very similar. The formation of a stratified layer bounded above and below by relatively well-mixed fluid is a feature observed in the
spin-up experiments from rest of [4, 7] and [5] where the fluid was stratified by salinity.

Several snapshots of the adjustment of the thermally-stratified flow from one state of rotation to another showing the formation of three-dimensional vortex structures is presented in figure 8, but the spatio-temporal nature of this evolution is better appreciated from movie 7 (available in the online version). The temperature profile on the left is shown on the \( \theta = 0 - \pi \)-plane. The vortex structure colored by temperature and identified by the \( Q \)-criterion of [36] is shown on the middle of the figure and a plan view of the same vortex on the right. The \( Q > 0 \) identifies vortices as flow regions where the second invariant of \( \nabla \mathbf{u} \) is positive. In an incompressible flow \( Q \) is a local measure of the excess rotation rate relative to the strain rate, i.e., if \( \mathbf{S} \) and \( \mathbf{\Omega} \) are the symmetric and antisymmetric components of \( \nabla \mathbf{u} \) then the second invariant can be written as 
\[
Q = \frac{1}{2} \left( \| \mathbf{\Omega} \|^2 - \| \mathbf{S} \|^2 \right) \ [37].
\]
The growth of the isotherms around the corner halts at \( \tau \approx 7 \) and the front becomes stationary. During this growth, the vortex core remains axisymmetric, but small disturbances appear to grow on and under the surface as shown in figure 8(b). These small-scale structures within the corner regions correspond to the pockets of relative cold and warm fluid depicted in figure 6(b).

The vortex structure correlates well with the vertical vorticity \( \omega_z \) shown at different horizontal planes in figure 9. At \( \tau = 0 \) the vertical vorticity is equal to \(-2\) in the entire flow domain as it is in solid-body rotation. When \( \tau < 5 \) the vorticity distribution is axisymmetric and forms a system of smooth con-
centric rings. The vorticity is positive near the sidewall and retains negative values near the center. The distribution of vorticity in the radial direction is not monotonic after $\tau \sim 1$. As time progresses ($\tau = 2 - 5$) the vorticity rings of opposite signs alternate with each other at some distance from the sidewall (see also figure 8 and movies 8-10). Around $\tau = 6 - 7$, the rings start disintegrating into small-scale patches of positive and negative vorticity shown in figure 9(a) at $\tau = 7$. This process is more vigorous at the lower vertical levels than at the top. The flow retains a solid-body rotation (concentric vorticity rings) near the axis of rotation until $\tau \sim 10$. The vorticity distribution acquires a shape of spiral bands around $\tau = 15$ followed by the development of large-scale eddies at about $\tau = 20$. The vorticity distribution is very coherent at various vertical levels (see figure 9, $\tau = 34$ and movies 8-10) including the lowest level $z = 0.01$, which is well inside the bottom Ekman layer ($\delta = 0.054$). After $\tau \sim 20$ the highly distorted (asymmetric) flow near the sidewall progresses forms three distinctive cyclonic eddies (at $\tau = 22$) which undergo further merging forming two large cyclones by $\tau = 25$. At later times the vertical coherence of the flow pattern is lost and the columnar eddies disintegrate into a system of smaller vortices.

A comparison of the rate of growth of the first four instability modes ($n = 1, \cdots, 4$) to the decay of the mean current ($n = 0$) is shown in figure 10. The energy curve of the mean current decreases monotonically in time until it is overcome by the fastest growing modes $n = 1, 2$ at about $\tau \approx 40$. All other modes stay below the mode $n = 0$ at all times, although experiencing
oscillations at late times.

The time evolution of each term of the perturbation energy equation (13) allows us to determine the contribution to the instability of the barotropic ($H_1$), baroclinic ($H_2$), centrifugal ($H_3$) and viscous dissipation ($H_4$) terms. The flow was not initially perturbed and therefore the small noise associated with the round-off errors of the numerical discretization triggered the three-dimensional instabilities. Figures 11(a)-(b) illustrate the time history of each individual term $H_i$ of the rate of change of kinetic energy and $de/dt$ respectively. The kinetic energy term $e(\tau)$ in figure 11(c) demonstrates a small peak at time $\tau \approx 7$ reaching a maximum at $\tau = 30$. The centrifugal term ($H_3$) remains negligible over the entire simulation time interval, and does not influence the flow dynamics, which is governed by the interplay among the barotropic ($H_1$), baroclinic ($H_2$) and viscous dissipation ($H_4$) terms. At early spin-up times the barotropic term, which is positive, serves as a source of azimuthal instabilities through the mean current shear. However, at later times it acquires both positive and negative values and even experiences undulations about the zero level. During some time intervals the perturbations are amplified by absorbing the energy from mean current. The baroclinic (gravity) term reaches peak values at $\tau \approx 20$. The release of the potential energy is accompanied by the oscillations of both barotropic and baroclinic terms (the local maxima of the baroclinic oscillations are correlated with the local minima of barotropic oscillations). According to figure 11(c), the energetic stage of the flow evolution ends by $\tau = 135$ and the final state consist
Figure 12: Case DIR: Isotherms on the planes $\theta = 0 - \pi$; at $\tau = 0$ there are 32 linearly spaced contour levels in the range $T_H \in [0, 1]$ showing the formation of the corner regions and the motion after the vortex core is formed. The region shown is $r \in [0, 6.67]$ and $z \in [0, 2]$. Movie 11, available in the online version, shows the spatio-temporal characteristics for the isotherms on the planes $\theta = 0, \pi$ over 145 rotation periods at a rate of 10 frames per second, with each frame being 1 rotation period apart.

of irregular eddies shown in figure 8(d) and movie 7. The evolution of instabilities due to the interaction of the vertical and horizontal shears (terms $H_1$ and $H_2$ respectively) observed in this numerical simulation is similar to the observations of instabilities in the laboratory experiments of [5] and [8].
(a) Vertical profiles of $u_r$ at $r = 5.5$ and times $\tau = 1$ ($\circ$), 3 ($\circ$), 7 ($\nabla$), 20 ($\triangle$).

(b) Vertical profiles of $T_H$ at $r = 0.1$ and times $\tau = 0$ ($\cdots$), 3 ($\circ$), 20 ($\triangle$), 45 ($\diamond$), and 120 ($\times$).

(c) Vertical profiles of $T_H$ at $r = 4.5$ and times $\tau = 0$ ($\cdots$), 3 ($\circ$), 20 ($\triangle$), 45 ($\diamond$), and 120 ($\times$).

(d) Vertical profiles of $T_H$ at $r = 6.5$ and times $\tau = 0$ ($\cdots$), 3 ($\circ$), 20 ($\triangle$), 45 ($\diamond$), and 120 ($\times$).

Figure 13: Radial velocity $u_r$ and temperature profiles $T_H$ at different radial locations and $\theta = 0$ for DIR. Note that the solid line in (a) indicates the depth of the Ekman layer.
Figure 14: Case DIR: Temperature and vortex structure identified by the isosurfaces of $Q = 0$ colored by temperature. The figures on the left correspond to $T_H \in [0 - 1]$ and on the middle/right to the vortex structure. The region shown is $r \in [0, 6.67]$ and $z \in [0, 2]$. Movie 12, available in the online version, shows the spatio-temporal characteristics for the isotherms and vortex structure. The animations run over 100 rotation periods at a rate of 4 frames per second, with each frame being 1 rotation period apart.
Figure 15: Case DIR: Axial vorticity $\omega_z$; there are 7 positive (solid/black) and 7 negative (white/dashed) linearly spaced contour levels in the range $\omega_z \in [-1, 1]$. The region shown is $r \in [0, 6.67]$ and $z \in [0, 2]$. Movies 13-15, available in the online version, show the spatio-temporal characteristics for the axial vorticity at different $z$-levels.

Figure 16: Case DIR: Time evolution of different energy modes $E_n$: $n = 0$ (——); $n = 1$ ($\circ$); $n = 2$ (—); $n = 3$ (·—); $n = 4$ ($\diamond$).
Figure 17: Case DIR: Time evolution of (a) $H_i$-terms in the rate of change of kinetic energy of azimuthal perturbations; barotropic term $H_1$ (——); baroclinic term $H_2$ (—·—); centrifugal term $H_3$ (—); viscous dissipation term $H_4$ (—··—), (b) the rate of change of kinetic energy $de/dt$ and (c) the kinetic energy $e(\tau)$.
4.3 Nonaxisymmetric spin-up with specified temperature boundary conditions: Case DIR

The evolution of the temperature field on the planes $\theta = 0 - \pi$ over several rotation periods is shown in figure 12 and movie 11 for $(\Gamma, \epsilon, Bu) = (6.67, 0.727, 0.379)$. These are the same parameters as in the NEU but with specified constant temperatures $T_H = 1, 0$ at the top and bottom walls respectively. Initially, there are no radial temperature gradients and the isotherms are horizontal. At the outset of spin-up, the isotherms around the corner regions deform due to the Ekman transport in the bottom boundary layer towards the outer sidewall. Since the bottom boundary acts as a source of dense fluid by the constant temperature boundary condition, a significant contribution to the temperature anomalies is due to the vertical advection of temperature in the corner regions, which drastically enhances the horizontal temperature gradient.

The downwelling motion in the central part of the cylinder coupled with the specified constant temperatures boundary conditions force the isotherms around $r = 0$ to be severely compressed in the vertical direction ($\tau \approx 7$). The stratification near the bottom at $r = 0$ increases from its initial state due to downwelling. As the fluid from the corner regions flushes back towards $r = 0$, the highly stratified core acts as a restituting force that delays the development of instabilities. The generation of internal waves is only evident at $\tau = 85$ and only at late times the temperature gradient recovers its initial linear profile (see movie 11 available online).
The formation and development of the Ekman bottom boundary-layer flow at \((r, \theta) = (5.5, 0)\) is depicted in figure 13(a). The horizontal solid line marks the thickness of the Ekman layer \(\delta\). The vertical profiles of the radial velocity \(u_r\) show an increased fluid transport in the meridional plane at early spin-up times \((\tau \leq 1)\) followed by a gradual decrease in both the Ekman transport and amplitude of \(u_r\). The value of \(u_r\) becomes negligible within the Ekman layer at about 18-20 rotation periods. Figures 13(b)-(d) show the vertical profiles of temperature \(T_H(z)\) on the plane \(\theta = 0\) for \(r = 0.1, 4.5\) and 6.5. The dashed lines in the figures depict the background temperature profile at time \(\tau = 0\). Near the axis of rotation \((r = 0.1)\) the temperature profiles for \(\tau > 0\) lie beneath the initial temperature contour due to downwelling. The largest deviation from the initial linear profile occurs after about 18-20 rotation periods. At very late times \((\tau > 85)\) the initial temperature gradient is almost recovered.

Snapshots of the formation of three-dimensional vortex structures are presented in figure 14. Movie 12 (available in the online version) shows the evolution of the spatio-temporal nature the spin-up and corresponds to the same figure. The temperature profile on the left is shown on the \(\theta = 0 - \pi\)-plane. The vortex structure is colored by temperature and identified by the isosurfaces of \(Q = 0\) and shown in the middle of the figure; a plan view of the same vortex structure is depicted on the right. During the growth of the corner regions \((\tau < 7)\), the vortex core remains axisymmetric with small disturbances under the surface. Clearly the amount of small-scale structures
within the corner regions is less than in NEU as can be seen by comparing figures 14(b) and 8(b) showing the perturbations on the boundary between the vortex core and the bottom wall (top view). The contour levels of axial vorticity $\omega_z$ of figure 15(a) ($\tau = 7$) also illustrate the Ekman layer instabilities generated on this boundary. The wobbling of the inner core, associated with the formation of spiral bands at $\tau = 15$, amplifies in time until a dumb-bell shape structure composed of two anticyclones manifests itself around $\tau = 30$ (see figures 14 and 15, $\tau = 34$ and movies 12–15) The vorticity patterns at different $z$-levels show two cyclonic eddies that accompany anticyclones at $z = 0.01$, but on the upper levels $z = 1, 1.9$ these eddies are only seen at late times. The instability mechanism seems to be effective with the appearance of the elliptic vortex structure combined with the baroclinic waves, enhancing the wobbling of the flow.

The rate of growth of the first four instability modes ($n = 1, \cdots, 4$) in figure 16 is consistent with the evolution of the vortex structure and $\omega_z$ shown in figures 14 and 15 and movies 12–15. The monotonic decay of the mean current ($n = 0$) is also shown in the figure. The initial growth of the modes is suppressed at early times and achieves a local minimum at around $\tau \sim 30$, particularly $n = 4$. At about $\tau \approx 100$ the energy of the mean current is overcome by the fastest growing mode $n = 1$. Modes $n = 2, 3$ and 4 remain below the mode $n = 0$ at all times.

The time evolution of each term of the perturbation energy equation (13), the rate of change of kinetic energy and the kinetic energy of azimuthal per-
turbations are depicted in figure 17. Figures 17(a)-(b) illustrate the time history of each individual term $H_i$ of the rate of change of kinetic energy and $\frac{de}{dt}$ respectively. The kinetic energy term shown in figure 17(c) demonstrates a small peak at time $\tau \approx 7$ becomes negligible at around $\tau = 30$ (the flow becomes almost axisymmetric), followed by a continuous growth until it reaches a global maximum around $\tau \approx 90 - 100$ continued by a monotonic decay until it becomes negligible at late times $\tau > 180$. It is evident from figure 17 that the centrifugal term ($H_2$) remains negligible over the entire simulation.

At early spin-up times both the barotropic ($H_1$) and baroclinic ($H_2$) terms, which are positive, are a source of azimuthal instabilities through the mean current shear. At late times, the barotropic term acquires both positive and negative values and experiences undulations about the zero level. The baroclinic (gravity) term reaches a local maximum at $\tau = 7$ and a global maximum at $\tau \approx 85$. At around $\tau = 7$ the flow is forced to an axisymmetric state due to the stabilizing role of the stratified core, but notice that the vortex structure has already lost its axisymmetry near the bottom wall, and it only shows an axisymmetric character well above the bottom boundary. The vortex core seems to lose its stability through a resonant mechanism generated at the interface of its surface and the bottom wall. The viscous dissipation cannot counteract a much vigorous release of the potential energy at $\tau \approx 85$. The release of the potential energy is accompanied by the oscillations in both barotropic and baroclinic terms (the maxima of the baroclinic
oscillations are also correlated with the minima of barotropic oscillations). The energetic stage of the flow evolution spans for a long time in DIR and only by the time \( \tau \approx 180 \) all energy terms essentially reduce to zero. At this time the flow shows an irregular system of weak eddies (see movie 12).

### 4.4 Comparison between NEU and DIR cases

In order to explain why NEU develops eddies earlier than DIR let us examine the baroclinic contribution to vorticity, which is proportional to \( \nabla T_H \times \nabla p \). This vector is also proportional to the angle between surfaces of constant temperature and surfaces of constant pressure. Figure 18 depicts the isotherms and isobars for NEU and DIR at \( \tau = 7 \) when the corner regions have matured. The dots shown in figure 18 are located around the boundary between the corner regions and vortex core. Clearly, the isotherms and the isobars around the vortex core are nearly orthogonal in NEU, whereas in DIR, the isotherms and isobars are almost parallel. The contribution to the vorticity due to the vertical shears are more pronounced in NEU than in DIR, and the growth of eddies in DIR is delayed due to the relative strong stratification around \( r = 0 \) which acts as a restoring mechanism. Previous studies have implicitly assumed that the destabilizing effect is mainly baroclinic (the shear is mainly vertical). However, as shown in figure 11 and 17, both vertical and horizontal shears contribute to the instability. The ratio of the barotropic to the baroclinic terms \( H_1/H_2 \) is proportional to \( h/L = \Omega/N \) at the time when the corner regions mature [7, 5]. The numerical value of this ratio for NEU at
around $\tau \approx 10$ is $H_1/H_2 = 0.177/0.542 \approx \tan(20^\circ)$, whereas $\Omega/N \approx \tan(21^\circ)$ (see figure11). In DIR, the initial disturbance is caused by the combined effect of vertical and horizontal shears where $H_1/H_2 = 0.051/0.132 \approx \tan(22^\circ)$ with $\Omega/N \approx \tan(21^\circ)$ at $\tau \approx 10$; but the subsequent growth of instabilities (around $\tau \approx 40$) is purely baroclinic, as shown in figure 17. These results imply that the non-axisymmetric instability of the spin-up flow in a circular cylinder is strongly influenced by the imposed temperature boundary conditions on top/bottom walls of the cylinder.

5 Discussion and conclusions

We have conducted three-dimensional time-dependent numerical simulations of nonlinear spin-up of a thermally stratified fluid in a circular cylinder taking into account both fixed temperature and thermally insulated boundary conditions. The latter boundary condition is more appropriate to use in comparing with previous salt-stratified laboratory experiments.

The evolution of stratified spin-up has been characterized by two distinct stages. In the first stage we found the existence of the bottom Ekman layer, which pumps the stratified fluid from the interior into the corner regions that remained axisymmetric. The instantaneous vertical density profiles near the outer sidewall and the core of the cylinder demonstrate the regions of strong upwelling and downwelling respectively. Because of the vigorous stirring inside the corner regions, the fluid tends to homogenize there.

In our simulations, the formation time of the axisymmetric corner re-
Figure 18: Isotherms (top) and isobars (bottom) on the planes $\theta = 0 - \pi$; at $\tau = 0$ there are 15 linearly spaced contour levels in the range $T_H \in [0, 1]$. The region shown is $r \in [0, 6.67]$ and $z \in [0, 2]$. The symbol $\bullet$ indicates a reference point for comparing the angle formed by the isotherms and isobars at that particular location.
regions is \( \tau_{su} \approx 7.7 \) rotation periods, the homogeneous spin-up time is \( \tau_{su} = (2E)^{-1/2}/\pi \approx 5.9 \) and the estimate of [7] \( \tau_{su} = 1.3/(\Gamma \sqrt{2EN}) \approx 9.8 \) rotation periods. The maximum height and radius of the corner regions are consistent with the theoretical estimates \( h = 2/3Bu \) and \( L = 2\Gamma/3 \) of [7].

In the second stage, the flow becomes unstable depending on the relative values of \( \Gamma, \epsilon \) and \( Bu \) but the subsequent development of the instability strongly depends on the specified temperature boundary conditions on the top and bottom walls of the cylinder (the sidewall is always thermally insulated). When the end-walls are insulated (case NEU), the axisymmetry is lost via a baroclinic instability of the corner regions and subsequent propagation of instability towards the inner region of the cylinder. These observations were also found in the laboratory experiments of [4, 8, 5, 9, 10] and [11]. When the temperatures at the top and bottom walls are specified (case DIR), the spin-up flow loses its axisymmetry through the wobbling of the inner core in a manner that is reminiscent of an elliptical instability.

The numerical results for HOM suggest that in order to develop eddies at late spin-up times (considering that our simulations are in the transient Ekman boundary layer regime) a baroclinic instability of the corner region is necessary. The azimuthal instability in this regime seems to be sensitive to the specific values of the Burger and Rossby numbers as evidence by the results from LBU and SRO. Notice that the value of the Rossby number in SRO (see table 1) is still big enough to be considered in the nonlinear regime of stratified spin-up. For similar values of Burger and Rossby numbers
$(Bu = 0.38$ and $\epsilon = 0.18$) non-axisymmetric instabilities were observed in the experiments of [10]. Therefore, the influence of the aspect ratio $\Gamma$ and the Ekman number $E$ play an important role in the formation of these large columnar eddies.

In conclusion, this numerical study has shown that thermally-stratified spin-up flows may develop non-axisymmetric instabilities that lead to the formation of large-scale columnar vortices in high Rossby number spin-up flow at late times. To the best of our knowledge, previous studies where the stratification was created by temperature have reported axisymmetric flow patterns only [13, 14, 15, 17, 18, 19]. Furthermore, we are not aware of any three-dimensional numerical simulation of stratified spin-up in which columnar eddies have been observed.

By characterizing the azimuthal instabilities without introducing any simplification we were able to determine to what extent an insulating boundary condition changes the time-dependent emergence of the instability. The computation of the time evolution of each term of the perturbation energy equation allowed us to determine the contribution to the instability of the barotropic and baroclinic terms. Hence, we were able to identify the mechanisms responsible for the subsequent growth of eddies at the late stages of flow development when using Neumann or Dirichlet boundary conditions in a numerical setup. The results from our numerical simulations are in excellent agreement with previous laboratory experiments of stratified spin-up.

Finally, there are many aspects of nonlinear spin-up flow which require
more exploration, and this study provides the framework for further investigations. One of them is the study in parameter space \((\Gamma, Bu)\) for fixed \(\epsilon\) of incremental spin-up in cylindrical and annular geometries with flat and sloping bottoms, which will be the subject of forthcoming papers.

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References


